## FSCH/FSPT Registration Quiz 2024 Results V1.0

## Information:

Unlike stated in FSCH Handbook 2024 CH 2.1.3, protest time ends 4 hours later, meaning 2024-01-27 17:00 CET.
Send your protest(s) to geral@formulastudent.pt irrelevant of your intended participation in FSCH, FSPT or both.

## Q1 (CV \& EV)

A chocolate manufacturer is producing a new type of chocolate bar with a special formulation. The chocolate is initially melted and poured into a mould at a temperature of $50^{\circ} \mathrm{C}$. The chocolate bar is then left to cool in a room with a constant temperature of $20^{\circ} \mathrm{C}$. The manufacturer wants to determine the time it takes for the chocolate to cool down to a safe handling temperature of $30^{\circ} \mathrm{C}$.
Given that the chocolate follows Newton's Law of Cooling, the manufacturer has conducted preliminary experiments and determined that the cooling rate constant (k) for this chocolate formulation is 0.02 per minute.
Determine the time it takes for the chocolate to cool down from $50^{\circ} \mathrm{C}$ to $30^{\circ} \mathrm{C}$.
Answer in min and provide the value with 2 decimal places, e.g. 12.34.
Answer: 54.93
Newton's Law of Cooling: dTdt=k(T-T amb)
T amb $=20^{\circ} \mathrm{C}$
so $T(t)=20+30 \mathrm{e}-0.02 \mathrm{t}$
solving for $t$ with $T(t)=30^{\circ} \mathrm{C}$ gives $\mathrm{t}=-\ln (13) 0.02=54.93$ min

## Q2 (CV \& EV)

Knowing that the member AC is under a force of -25 kN , what is the force in the element HG ? Force R is an unknown horizontal force applied on point H .
Answer in kN and provide the value with 1 decimal place, e.g. 12.3.
Follow the sign convention "-" for a compressive force and " + " for tensile, e.g. -12.3 or 12.3.


Answer: -35.4
Assuming positive x from left to right and positive y from down to up (coordinate system not relevant for solution)
R_A_x (x component of reactive force at A) = -f_AC $=25 \mathrm{kN}$
Sum of forces along $x$ :
R_A_x $=\sin (45)^{*} 100 \mathrm{kN}-\mathrm{R}=>\mathrm{R}=45.71068 \mathrm{kN}$
Sum of moments around $A$
R_G_y * $12=25$ * $3+R^{*} 3+100$ * $\sin (45) * 3-100 * \cos (45) * 2=>R_{-} G \_y=35.355 \mathrm{kN}$
R_G_y = - f_HG => f_HG = -35.355 kN

## Q3 (CV \& EV)

Your racecar is equipped with four independent suspensions. The front and rear motion ratios are 0.8 and 0.75 , respectively. The front and rear spring stiffnesses are $16 \mathrm{~N} / \mathrm{mm}$ and 18 $\mathrm{N} / \mathrm{mm}$, respectively. The tire stiffness is $75 \mathrm{~N} / \mathrm{mm}$. Under an aerodynamic load applied at the vehicle centre of gravity, the wheel travel relative to a static position is the same for the 4 wheels. What is the static longitudinal weight distribution of the car? (Assume that the vehicle is coasting, i.e., no longitudinal force is applied by the wheels on the ground).
Answer as \% of mass on the front axle and provide the value with 1 decimal place, e.g. 12.3.
Answer: 43.9
Front wheel rate $=$ Front spring stiffness $/$ front motion ratio $=16 / 0.8^{\wedge} 2=25 \mathrm{~N} / \mathrm{mm}$
Rear wheel rate $=$ Rear spring stiffness $/$ rear motion ratio $=18 / 0.75^{\wedge} 2=32 \mathrm{~N} / \mathrm{mm}$

$$
\begin{array}{ll} 
& \text { Downforce * } \frac{\text { fraction weight front }}{\text { Front wheel rate }}
\end{array}=\text { Downforce * } \frac{\text { fraction weight rear }}{\text { Rear wheel rate }}
$$

Note that the drag force does not cause any longitudinal mass transfer since it is not balanced by an equal and opposite force applied in the tires, i.e., the drag force causes deceleration of the vehicle instead of mass transfer.

## Q4 (CV \& EV)

The figure below depicts an Improved Howland Current Pump circuit. Assume that Vin- is connected to ground, 0 V , and Vin+ is 5 V . For R1 $=\mathrm{R} 2=\mathrm{R} 3=1 \mathrm{k} \Omega$ and $\mathrm{R} 4=100 \Omega$, compute the magnitude of the output current lout.


Answer in mA and provide the value with 1 decimal place, e.g. 12.3.
Answer: 50.0
Formulas for an improved howland pump circuit:
Iout $=(G \times(\operatorname{Vin}+-\operatorname{Vin}-)) / R 4$,
$G=R 3 / R 1 ; \quad R 3 / R 1=(R 5+R 4) / R 3$
$G=1 k / 1 k=1 ; 1=(R 5+R 4) / R 3<=>R 5=1000-100=900 \Omega$
Iout $=1^{*}(5-0) / 100=0.05 A=50.0 \mathrm{~mA}$

## Q5 (CV \& EV)

A structural engineer needs to design a thin simply supported rectangular beam that experiences a point load of 500 N in the middle of its length. The beam is 200 mm long and 50 mm wide. The engineer considers two materials for the panel: aluminium and quasiisotropic carbon fibre. The aluminium used has a Young's Modulus of 70 GPa and a density of $2.7 \mathrm{~g} / \mathrm{cm}^{\wedge} 3$. The composite used has a Young's Modulus of 220 GPa and a density of 1.26 $\mathrm{g} / \mathrm{cm}^{\wedge} 3$. The environmental impact of the beam aluminium used is 8 kgCO 2 per kilo of aluminium and the one of the carbon is 26 kgCO 2 per kilo of composite.
What is the lowest possible CO2 emission out of these two options while having a beam maximum deflection of 3 mm .
a) Aluminium
b) Composite

Answer in kgCO 2 and provide the value with 3 decimal places, e.g. 12.345.
Answer: 0.986
Deflection: $\frac{500 * 200^{3}}{48 E I}$
Inertia: $I=\frac{50 t^{3}}{12}$
So $t>\sqrt[3]{\frac{500 * 12}{3 * 48^{*} 50 * E}} * 200$
Aluminium: $\mathrm{t}=4.56 \mathrm{~mm} \rightarrow$ mass $=\left(4.56^{*} 200 * 50\right)^{*} 2.7 \mathrm{e}-3=123.12 \mathrm{~g}$ so the environmental impact is:
$8 \mathrm{e}-3 * 123.12=0.986 \mathrm{kgCO} 2$
Composite: $\mathrm{t}=3.12 \mathrm{~mm} \rightarrow$ mass $=\left(3.12^{*} 200^{*} 50\right)^{*} 1.26 \mathrm{e}-3=39.31 \mathrm{~g}$ so the environmental impact is:
$26 \mathrm{e}-3 * 39.31=1.022 \mathrm{kgCO} 2$

## Q6 (CV \& EV)

Your racecar is performing a steady-state corner with 8 metres radius at a speed of $10.2 \mathrm{~m} / \mathrm{s}$. The vehicle has a longitudinal weight distribution of $50 \%$ front / $50 \%$ rear, parallel steering ( $0 \%$ ackermann), and 0.5 degrees rear wheel toe in. Knowing that the slip angle of the rear inside wheel is 4.6 degrees, how much toe is needed on the front wheels to ensure that these have equal slip angles $\left(\alpha_{\mathrm{fi}}=\alpha_{\mathrm{fo}}\right)$ ?
$\mathrm{l}_{\mathrm{f}}=0.8 \mathrm{~m}, \mathrm{l}_{\mathrm{r}}=0.8 \mathrm{~m}, \mathrm{t}=1.2 \mathrm{~m}, \delta=12 \mathrm{deg}$
Toe in is considered positive, toe out is considered negative. Answer in deg and provide the value with 1 decimal place, e.g. 12.3.


Answer: -0.5
Assuming x is positive from rear to front and y is positive from right to left (coordinate system
not relevant for solution)
Yaw_rate $=$ velocity $/$ radius $=10.2 / 8=1.275 \mathrm{rad} / \mathrm{s}$
Vx_RI $=$ Vx - Yaw_rate*t/2 $=9.435 \mathrm{~m} / \mathrm{s}$
Vy_RI $=-\tan \left(\right.$ alfa_RI + toe_rear) ${ }^{*} V x \_R I=-\tan (5.1 \mathrm{deg})^{*} 9.435=0.84205 \mathrm{~m} / \mathrm{s}$
Vx_FI $=$ Vx_RI $=9.435 \mathrm{~m} / \mathrm{s}$
$V y_{\text {_ }} \mathrm{FI}=\mathrm{Vy}$ _RI + Yaw_rate $*(\mathrm{Ir}+\mathrm{If})=-\tan (5.1 \mathrm{deg})^{*} 9.435+1.275 * 1.6=1.19795 \mathrm{~m} / \mathrm{s}$
alfa_FI $=12-\operatorname{atan}(1.19795 / 9.435)-$ toe_front $=4.76-$ toe_front
Vx_FO $=$ Vx + Yaw_rate ${ }^{*} / 2=10.965 \mathrm{~m} / \mathrm{s}$
$V y$ _FO $=\mathrm{Vy}$ _FI $=1.19795 \mathrm{~m} / \mathrm{s}$
alfa_FO $=12-\operatorname{atan}(1.19795 / 10.965)+$ toe_front $=5.76+$ toe_front
alfa_FI $=$ alfa_FO $=>$ toe_front $=-0.5 \mathrm{deg}$

## Q7 (CV \& EV)

Last year's car had a sprocket on the output shaft of the engine with 16 teeth. Connected to this sprocket was a chain that drove the output gear resulting in a gear ratio of 2.5. This year, the team wants to maintain the same sprocket but in the meanwhile the supplier has discontinued the previously used output gear and the closest one in stock has 2 extra teeth. What is the new gear ratio if the team chooses to use it?
Answer is unitless, provide the value with 1 decimal place, e.g. 12.3.
Answer: 2.6
Old car: $Z 1=16 ; \quad i 1 / 2=2,5$
New car: Z1=Z3=16; Z4=Z2+2
Z2= Z1*i $^{*} 1 / 2$
Z2 $=16 * 2,5$
$Z 2=40$

Z4= Z2+2
Z4 $=40+2$
Z4 $=42$
i3/4= Z4/Z3
i3/4 $=42 / 16$
$i 3 / 4=2,625 \rightarrow 2,6$

## Q8 (CV \& EV)

From these options, what is the lightest possible section for the Main Hoop Bracing?

Round tube Outer diameter $=25 \mathrm{~mm}$, thickness $=1.2 \mathrm{~mm}$
Round tube Outer diameter $=20 \mathrm{~mm}$, thickness $=1.5 \mathrm{~mm}$
Squared tube side $=1$ ", thickness $=3 / 64^{\prime \prime}$
Round tube Outer diameter $=32 \mathrm{~mm}$, thickness $=1.2 \mathrm{~mm}$
X Squared tube side $=7 / 8^{\prime \prime}$, thickness $=1 / 16^{\prime \prime}$
Round tube Outer diameter $=28 \mathrm{~mm}$, thickness $=1.6 \mathrm{~mm}$
Option 1, 2, $3 \& 4 \rightarrow$ not enough inertia or too thin
Squared tube $7 / 8 " \times 1 / 16^{\prime \prime} \rightarrow(25,4 \times 7 / 8)^{\wedge} 2 \mathrm{~mm} 2-(25,4 \times 7 / 8-2 \times(25.4 \times 1 / 16))^{\wedge} 2 \mathrm{~mm} 2=$ 131.0 mm 2

Rounded tube $28 \times 1.6 \rightarrow 25,4^{\wedge} 2 \mathrm{~mm} 2-(25,4-2(25.4 \times 3 / 64))^{\wedge} 2 \mathrm{~mm} 2=132.7 \mathrm{~mm} 2$

## Q9 (CV \& EV)

Compute the energy retrieved from a 2 F supercapacitor charged to 100 V and discharged at constant current down to 50 V ?

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X 7.5 kJ
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© 10 kJ
All wrong
○ 5 kJ
2.5 kJ

○ 3.75 kJ
$E=0.5^{*} C^{*}\left(\right.$ Vinitial $^{2}-$ Vfinal $\left.^{2}\right)$
$E=0.5^{*} 2^{*}\left(100^{2}-50^{2}\right)=0.5^{*} 2^{*}(100000-2500)=1^{*}(7500)=7.5 \mathrm{~kJ}$

## Q10 (CV)

What is the vibration frequency of a four-cylinder in-line engine at 4500 rpm at the dominant engine order that causes the typical four-cylinder hum?
Answer in Hz and provide the value with 0 decimal places, e.g. 12.
Answer: 150
"In the widely used four-cylinder in-line engines, the vibrations of the second engine order are dominant; this engine design owes the typical four-cylinder hum to them."
[Entkopplungselemente in der Fahrzeugtechnik] $\rightarrow$ nOrd=2 (It can also be found on the internet.)
$\mathrm{f}=\mathrm{nOrd}{ }^{*} \mathrm{r}^{*} \mathrm{~Hz} /(60 * 1 / \mathrm{min})$
$f=2^{*} 4500 *(1 / \mathrm{min})^{*} \mathrm{~Hz} /\left(60^{*}(1 / \mathrm{min})\right)$
$\mathrm{f}=9000 \mathrm{~Hz} / 60$
$\mathrm{f}=150 \mathrm{~Hz}$

## Q11 (CV)

## Which statement is right?

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Only fuel lines which are rated for temperatures of maximum of }12\mp@subsup{0}{}{\circ}\textrm{C}\mathrm{ are allowed to use between fuel tank and fuel rai and return lines.
Only fuel lines which are rated for temperatures of at least \(100^{\circ} \mathrm{C}\) are allowed to use between fuel tank and fuel rail and return lines.
Fuel lines designed for temperatures of at least \(120^{\circ} \mathrm{C}\) may only be used between the fuel tank and the fuel distributor.
Fuel lines designed for temperatures of at least \(200^{\circ} \mathrm{C}\) may only be used between the fuel tank and the fuel distributor.
* Only fuel lines which are rated for temperatures of at least \(120^{\circ} \mathrm{C}\) are allowed to use between fuel tank and fuel rail and return lines
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CV 2.4.1

## Q12 (CV)

Racing engines (for motorsports) often run at high mean piston speed and high compression ratio (i.e. high bmep), trading low engine displacement and weight for high wear and low Mean Time Between Failures. Consider a naturally aspirated 4-stroke engine to deliver 65 kW at $8,400 \mathrm{rpm}$ with a mean piston speed of $18 \mathrm{~m} / \mathrm{s}$, a bmep of 12 atm , and 3 cylinders. Find the appropriate cylinder bore diameter for such an engine, in mm.
Consider 1 atm=101325 Pa.
Answer in mm and provide the value with 1 decimal place, e.g. 12.3.
Answer: 71.0

$$
V_{d}=\frac{W_{b}}{b m e p}=\frac{2 \dot{W}_{b}}{N \cdot b m e p}=\frac{2(65,000 \mathrm{~J} / \mathrm{s})(60 \mathrm{~s} / \mathrm{min})}{(8400 \mathrm{rpm})(12 \mathrm{~atm})\left(101,325 \mathrm{~J} / \mathrm{m}^{3} \cdot \mathrm{~atm}\right)}
$$

$=0.764 \times 10^{-3} \mathrm{~m}^{3}$
$S=\frac{\bar{U}_{P}}{2 N}=\frac{\left(18 \mathrm{~m}^{\mathrm{m}} / \mathrm{s}\right)\left(60^{\mathrm{s}} / \mathrm{min}\right)}{2(8400 \mathrm{rpm})}=0.0643 \mathrm{~m}$
$B=\left(\frac{4 V_{d}}{n_{c} \pi S}\right)^{1 / 2}=\left[\frac{4\left(0.764 \times 10^{-3} \mathrm{~m}^{3}\right)}{3 \pi(0.0643 \mathrm{~m})}\right]^{1 / 2}=0.0710 \mathrm{~m}=71.0 \mathrm{~mm}$

## Q10 (EV)

You have a battery in a 27s1p configuration, where each cell has a capacity of 15 Ah and 4.2 V maximum voltage. The cell discharge circuit uses a constant current of 500 mA to discharge individual cells when balancing is required. Your battery has currently an unbalance of 5\% SoC between the highest and lowest SoC cells. You want to perfectly balance your battery so that the difference between the highest and lowest cells is $0 \mathrm{~V} / 0 \% \mathrm{SoC}$. How much time will balancing take?
Answer in hours and provide the value with 1 decimal place, e.g. 12.3.
Answer: 1.5
Divide the charge difference by the current: $5 \% \times 15 \mathrm{Ah} / 0.5 \mathrm{~A}=1.5 \mathrm{~h}$

## Q11 (EV)

This year you want to double your accumulator voltage to match your new high voltage electrical motor. Assume you keep the same accumulator nominal energy and the same cells you used last year and change only the cell configuration (series/parallel). Complete the statement: For the same power profile at the battery output, the power dissipated in the new accumulator internal resistance is (.........) the previous accumulator.

O four times
O double
$X$ equal to
O half
O one fourth
Cells - Ecell (cell nominal energy), Vcell (cell nominal voltage), Rcell (cell internal resistance)

Battery old - Eold (old battery nominal energy), Vold (old battery total nominal voltage), Rold (old battery total internal resistance), (Sold)s(Pold)p (old battery series parallel configuration), Presold (old battery dissipated power in internal resistance)

Battery new - Enew (new battery nominal energy), Vnew (new battery total nominal voltage), Rnew (new battery total internal resistance), (Snew)s(Pnew)p (new battery series parallel configuration), Presnew (new battery dissipated power in internal resistance)

Power profile - Ppro (RMS power), Ipro (RMS current)

We want Vnew = 2*Vold => Snew = 2*Sold (eqA)
To keep Enew = Eold => Sold * Pold = Snew * Pnew (eqB)
From A and B we get Pnew = Pold/2 (eqC)
Rold = Rcell * Sold / Pold (eqD)
Rnew = Rcell * Snew / Pnew (eqE)
From A, B and E we get Rnew = Rcell * 2*Sold / (Pod/2) = Rcel * 4 * Sold/Pold => Rnew =
4*Rold
Ipro = Ppro / Vbat
Iproold = Ppro / Vold
Ipronew = Ppro / Vnew = Ppro / (2*Vold) => Ipronew = ½ * lproold
Pres = Rbat * ${ }^{\text {Ipro^2 }}$
Presold = Rold * Iproold
Presnew $=$ Rnew * Ipronew $=4^{*}$ Rold * ( $1 / 2$ * lprold) ${ }^{\wedge} 2$ =>
=> Presnew = Presold

## Q12 (EV)

Your task is the design of the control circuit for the TSAL. Which of the LEDs in the circuit shown can be used as the red TSAL? Select the option which lists all correct answers comma-separated.


OA
$\times$ B
OC
OD
A B B D
OA,C
OA, D
B, C, D
OC,D
O none
The NE555 has an output signal of 4.45 Hz with $92 \%$ duty cycle.
The CD4040 is a Ripple Counter, where the output frequency is divided by 2 every output.
So the frequency of $C$ and $D$ is too low. But for $A$, the duty cycle is inverted, and with $8 \%$ too low.
Thus, only B is correct.

## Q13 (EV)

You have a powertrain composed of a battery with an internal resistance of $0.2 \Omega$ and an OCV (Open Circuit Voltage) of 500 V , an inverter with an efficiency of $97 \%$, a single electric motor with an efficiency of $94 \%$, a chain transmission with a gear ratio of 4 (reduction of motor speed) and an efficiency of $98 \%$ and a differential with a gear ratio of 1 and an efficiency of $96 \%$. The vehicle is two wheel drive with a wheel radius of 0.3 m .
Consider no other losses.
At a given moment, during braking with energy recovery, the current entering the battery is 84 A and the vehicle speed is $70 \mathrm{~km} / \mathrm{h}$.
At that moment, how much torque is being produced by each wheel?
Answer in Nm and provide the value with 0 decimal places, e.g. 12.
Answer: 390

```
Vbat=OCV+I*R \(=500+84^{*} 0.2=516.8 \mathrm{~V}\)
Pbat \(=\|^{*}\) Vbat \(=43411,2 \mathrm{~W}\)
Pground \(=\) Pbat \(/(\) product of efficiencies \()=43411,2 /\left(0.97^{*} 0.94 * 0.98^{*} 0.96\right)=50606,3 \mathrm{~W}\)
Speed \(=70 \mathrm{~km} / \mathrm{h}=70000 / 3600=19.444 \mathrm{~m} / \mathrm{s}\)
\(\omega=\) speed / perimeter * \(2 \pi=19.444 /\left(2\right.\) * \(\left.0.3^{*} \pi\right)\) * \(2 \pi=64,814 \mathrm{rad} / \mathrm{s}\)
Pwheel \(=\omega^{*} \tau=\) Pground/2
\(\mathrm{T}=\) Pwheel \(/ \omega=50606,3 / 2 / 64,814=390 \mathrm{Nm}\)
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